

Two More Moon Tracking Computer Programs



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The first moon tracking computer program included here was rewritten from WA1JXN/WA3GPL and K5JL versions presented in earlier issues of the EME notes. Warren Butler, W2WD, wrote the program for TRS-80 level II BASIC(16K). Cassette copies of the program are available from Warren for the cost of the cassette and postage (approximately \$1.00).

The second program was written in FORTRAN IV by Geoffrey Grayer, G3NAQ. Again the WA1JXN/WA3GPL program served as the starting point for this effort.

[illegible]

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51Ø INPUT F(N), V(N), Y(N)
52Ø IF F(N)=Ø THEN 64Ø
53Ø NEXT N
54Ø GOTO 5ØØ
55Ø INPUT"DO YOU WANT HARDCOPY (YES/NO)";WW$
56Ø PRINT
57Ø PRINT"WHAT ARE THE GMT MONTH, DAY, YEAR, TIME BEGINNING, TIME ENDING?"
58Ø PRINT"USE THE FORMAT MM,DD,YYYY,TTTT,TTTT
REMINDER --- USE 4 DIGITS FOR YEAR!"
59Ø FOR N=1TO31
6ØØ INPUT F(N), V(N), Y(N), Q(N), S(N)
61Ø IF F(N)=Ø THEN 64Ø
62Ø NEXT N
63Ø GOTO 59Ø
64Ø N5=N-1
65Ø FOR N=1 TO N5
66Ø IF B$="YES" THEN 68Ø
67Ø GOTO 71Ø
68Ø E1=24ØØ
69Ø B=Ø
7ØØ GOTO 73Ø
71Ø E1=S(N)
72Ø B=Q(N)
73Ø M=F(N)
74Ø D=V(N)
75Ø Y=Y(N)
76Ø Y1=Y-(INT(Y/1ØØ)*1ØØ)
77Ø PRINT
78Ø IF WW$="YES" LPRINT
79Ø PRINT:CLS
8ØØ IF WW$="YES" LPRINT
81Ø PRINT"POSITION OF THE MOON ON ";M;"/";D;"/";Y1;" GMT FROM"" "W$
82Ø IF WW$="YES" LPRINT"POSITION OF THE MOON ON ";M;"/";D;"/";Y1;" GMT FROM"" "W
$
83Ø PRINT
84Ø IF WW$="YES" LPRINT
85Ø PRINT"GMT"TAB(11)"GHA"TAB(21)"DEC"TAB(35)"EST"TAB(47)"AZ"TAB(57)"EL"
86Ø IF WW$="YES" LPRINT"GMT"TAB(11)"GHA"TAB(21)"DEC"TAB(35)"EST"TAB(47)"AZ"TAB(5
7)"EL"
87Ø PRINT
88Ø IF WW$="YES" LPRINT
89Ø I1=2
9ØØ IF M>=3 THEN 98Ø
91Ø IF INT((Y-1853)/4)<11 THEN 94Ø
92Ø C1=-1
93Ø GOTO 95Ø
94Ø C1=Ø
95Ø J1=365*(Y-1853)+D+3Ø*(M+9)+INT((M+1Ø)/2)
96Ø J2=INT((Y-1853)/4)+1+C1
97Ø GOTO 1Ø9Ø
98Ø IF INT((Y-1852)/4)<11 THEN 1Ø1Ø
99Ø C1=-1
1ØØØ GOTO 1Ø2Ø

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1010 C1=0
1020 IF M=9 THEN 1060
1030 IF M=11 THEN 1060
1040 C2=0
1050 GOTO 1070
1060 C2=1
1070 J1=365*(Y-1852)+D+3*(M-3)+INT((M-2)/2)
1080 J2=INT((Y-1852)/4)+C1+C2
1090 J=J1+J2
1100 T1=J-17472.5
1110 D9=(B-INT(B/100)*100)+INT(B/100)*60
1120 D6=(E1-INT(E1/100)*100)+INT(E1/100)*60
1130 D7=D9-D6
1140 D8=D7-1
1150 IF D7>0 THEN 1170
1160 GOTO 1190
1170 IF D8=0 THEN 2150
1180 B=E1
1190 T=(B-INT(B/100)*100)/144+INT(B/100)/24
1200 T5=T1+T
1210 K1=((.751213+.036601102*T5)-INT(.751213+.036601102*T5))*P5
1220 K2=((.822513+.0362916457*T5)-INT(.822513+.0362916457*T5))*P5
1230 K3=((.995766+.0273777852*T5)-INT(.995766+.0273777852*T5))*P5
1240 K4=((.974271+.0338631922*T5)-INT(.974271+.0338631922*T5))*P5
1250 K5=((.0312525+.0367481957*T5)-INT(.0312525+.0367481957*T5))*P5
1260 L8=K1+.658*R5*SIN(2*K4)+6.289*R5*SIN(K2)
1270 L8=L8-1.274*R5*SIN(K2-2*K4)-.186*R5*SIN(K3)
1280 L8=L8+.214*R5*SIN(2*K2)-.114*R5*SIN(2*K5)
1290 L8=L8-.059*R5*SIN(2*K2-2*K4)-.057*R5*SIN(K2+K3-2*K4)
1300 K6=K5+.6593*R5*SIN(2*K4)+6.2303*R5*SIN(K2)-1.272*R5*SIN(K2-2*K4)
1310 L7=5.144*R5*SIN(K6)-.146*R5*SIN(K5-2*K4)
1320 LET D1=COS(L7)*SIN(L8)*.397821+SIN(L7)*.917463
1330 LET D1=ATN(D1/(SQR(1-D1^2)))
1340 G1=50+.5+((D1)/(.792))*D5
1350 G2=80+((D1)/(.808))*D5
1360 G3=141.5-((D1)*(.738))*D5
1370 G4=170.5-((D1)*(.857))*D5
1380 A2=COS(L7)*COS(L8)/COS(D1)
1390 A1=(COS(L7)*SIN(L8)*.917463-SIN(L7)*.397821)/COS(D1)
1400 A=ATN(A1/A2)
1410 GOSUB 1670
1420 R1=A
1430 L1=.065709822*T1
1440 L=T*24*1.02738+6.646055+(L1-INT(L1/24)*24)
1450 L=(L-INT(L/24)*24)
1460 G=(L/24)*P5-R1
1470 IF G<P5 THEN 1500
1480 G=G-P5
1490 GOTO 1530
1500 IF G<0 THEN 1520

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151Ø GOTO 153Ø
152Ø G=G+P5
153Ø H=L6-G
154Ø E3=cos(L5)*cos(H)*cos(D1)+sin(D1)*sin(L5)
155Ø E2=sqr(1-(E3*E3))
156Ø E=atn((E3/E2)-(1/(61.33*E2)))
157Ø F=atn(E3/E2)
158Ø IF E<Ø THEN 21ØØ
159Ø IF E>16**R5 THEN 21ØØ
16ØØ A2=sin(D1)/(cos(L5)*cos(F))
161Ø A2=A2-(sin(L5)/cos(L5))*(sin(F)/cos(F))
162Ø A1=sin(L5)*sin(D1)+cos(L5)*cos(D1)*cos(H)
163Ø A1=(sin(H)*cos(D1))/sqr(1-A1*2)
164Ø A=atn(A1/A2)
165Ø GOSUB 167Ø
166Ø GOTO 182Ø
167Ø IF A=Ø THEN 169Ø
168Ø GOTO 173Ø
169Ø IF A2<Ø THEN 171Ø
17ØØ GOTO 181Ø
171Ø A=P5/2
172Ø GOTO 181Ø
173Ø IF A>Ø THEN 179Ø
174Ø IF A2<Ø THEN 177Ø
175Ø A=P5+A
176Ø GOTO 181Ø
177Ø A=P5+(A-P5/2)
178Ø GOTO 181Ø
179Ø IF A2=>Ø THEN 181Ø
18ØØ A=A+P5/2
181Ø RETURN
182Ø IF (T-I1)>(2**I)/144Ø THEN 184Ø
183Ø GOTO 185Ø
184Ø PRINT
185Ø BS=INT(B+.5):BS$=":::##"
186Ø Z1=INT(A*D5*1Ø+.5)/1Ø
187Ø Z2=INT(E*D5*1Ø+.5)/1Ø
188Ø Z3=INT(G*D5*1Ø+.5)/1Ø
189Ø Z4=INT(D1*D5*1Ø+.5)/1Ø
19ØØ IF Z4<Ø THEN 2Ø3Ø
191Ø IF Z3<G1 THEN 2Ø3Ø
192Ø IF Z3>G2 THEN 194Ø
193Ø GOTO 197Ø
194Ø IF Z3<G3 THEN 199Ø
195Ø IF Z3>G4 THEN 2Ø3Ø
196Ø GOTO 2Ø1Ø
197Ø Y$="U"
198Ø GOTO 2Ø4Ø
199Ø Y$="W"
2ØØØ GOTO 2Ø4Ø

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2010 Y$="J"
2020 GOTO 2040
2030 Y$=" "
2040 ES=(INT(B+.5))-500
2050 IF ES<=0 THEN ES=ES+2400
2060 ES$="###"
2070 PRINT USING BS$;BS;:PRINT TAB(10)Z3TAB(20)Z4;Y$TAB(35)USING ES$;ES;:PRINT TAB(45)
    Z1TAB(55)Z2
2080 IF WW$="YES" LPRINT USING BS$;BS;:LPRINT TAB(10)Z3TAB(20)Z4;Y$TAB(35)USING ES$;
    ES;:LPRINT TAB(45)Z1TAB(55)Z2
2090 I1=T
2100 B=B+I
2110 Z=(B-INT(B/100)*100)-60
2120 IF Z<0 THEN 1110
2130 B=INT(B/100)*100+100+Z
2140 GOTO 1110
2150 NEXT N
2160 N=0
2170 PRINT
2180 PRINT
2190 PRINT "DO YOU WANT MORE INFORMATION (YES/NO)";
2200 INPUT D$
2210 IF D$="YES" THEN 280
2220 END

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POSITION OF THE MOON ON 5 / 19 / 79 GMT FROM W2WD

GMT	GHA	DEC	EDT	AZ	EL
*615	357.4	-10	*215	106	2.2
*630	1	-9.9	*230	108.4	4.9
*645	4.6	-9.9	*245	110.8	7.5
*700	8.2	-9.8	*300	113.4	10.1
*715	11.8	-9.8	*315	115.9	12.6
*730	15.4	-9.8	*330	118.6	15.1
*745	19.1	-9.7	*345	121.3	17.5
*800	22.7	-9.7	*400	124.2	19.8
*815	26.3	-9.6	*415	127.2	22.1
*830	29.9	-9.6	*430	130.3	24.3
*845	33.5	-9.6	*445	133.5	26.4
*900	37.1	-9.5	*500	136.9	28.4
*915	40.8	-9.5	*515	140.4	30.3
*930	44.4	-9.4	*530	144.1	32
*945	48	-9.4	*545	147.9	33.6
1000	51.6	-9.4	*600	151.9	35
1015	55.2	-9.3	*615	156.1	36.2
1030	58.8	-9.3	*630	160.4	37.3
1045	62.5	-9.2	*645	164.8	38.2
1100	66.1	-9.2	*700	169.3	38.8
1115	69.7	-9.1	*715	174	39.3
1130	73.3	-9.1	*730	178.6	39.5
1145	76.9	-9.1	*745	183.3	39.5
1200	80.5	-9	*800	188	39.3
1215	84.2	-9	*815	192.6	38.8
1230	87.8	-8.9	*830	197.1	38.2
1245	91.4	-8.9	*845	201.5	37.3
1300	95	-8.9	*900	205.8	36.2
1315	98.6	-8.8	*915	210	35
1330	102.2	-8.8	*930	214	33.5
1345	105.9	-8.7	*945	217.9	31.9
1400	109.5	-8.7	1000	221.5	30.2
1415	113.1	-8.6	1015	225.1	28.3
1430	116.7	-8.6	1030	228.5	26.4
1445	120.3	-8.6	1045	231.7	24.3
1500	123.9	-8.5	1100	234.8	22.1
1515	127.6	-8.5	1115	237.8	19.8
1530	131.2	-8.4	1130	240.7	17.5
1545	134.8	-8.4	1145	243.5	15.1
1600	138.4	-8.4	1200	246.2	12.6
1615	142	-8.3	1215	248.8	10.1
1630	145.6	-8.3	1230	251.4	7.6
1645	149.3	-8.2	1245	253.9	4.9
1700	152.9	-8.2	1300	256.3	2.3


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THIS PROGRAM IS DESIGNED TO CALCULATE THE AZIMUTH AND ELEVATION OF THE MOON
THIS IS A FORTRAN VERSION OF PROGRAM 3 OF THE EIMAC EME NOTE AS-49-6
ORIGINALLY WRITTEN BY LANCE COLLISTER WA3GPL, CONVERTED BY GEOFF GRAYER G3NAQ.
THE INPUT FORMAT IS AS FOLLOWS...

FIRST DATA CARD:
OPTIONAL IDENTIFICATION (A10), LAT. OF STATION DEGS.(I10), LAT. OF STATION
MINS. (I10), LONG. OF STATION DEGS. (I10), LONG. OF STATION MINS. (I10).

SECOND AND SUBSEQUENT DATA CARDS:
YEAR (I10), MONTH (I10), DAY (I10), START HRS.-MINS.(I10), STOP HRS.-MINS.(I10)
TIME INCREMENT MINS.(I10) - DEFAULT 10 MINS., MAXIMUM ELEVATION DEGS. (I10) -
MAY BE USED TO SELECT PRINTOUT ONLY WHEN THE MOON IS NEAR THE HORIZON -
DEFAULT 90 DEGS.

ALL TIMES ARE IN GMT USING THE 0000 TO 2400 HOUR SYSTEM.

A BLANK CARD DENOTES THE END OF THE DATA SET AND TERMINATES THE PROGRAM.

PRINTOUT IS SUSPENDED WHENEVER THE ELEVATION OF THE MOON IS NEGATIVE.

FOR FURTHER INFORMATION, REFER TO THE EIMAC NOTE.

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GEOFFREY H. GRAYEN G3NAQ
BRIGHTWALTON, BERKSHIRE
APRIL, 1978

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0001      INTEGER D,Y,C1,C2,B,Z,E1,D6,D7,D8,D9,GMT
0002      REAL    PI,P5,D5,R5,K1,K2,K3,K4,K5,L8,K6,L7,D1,A1,A2,A,L1,L,E3,E2
0003      REAL    L5,L6,I1
0004      REAL*4  JU
0005      DIMENSION IDENT(10),GMT(4)
0006      FNA(X)=AINT(X*05*10.+0.5)/10.
0007      FNB(X)=(X-AINT(X))*P5
0008      PI=3.1415926535
0009      P5=2.*PI
0010      D5=180./PI
0011      R5=PI/180.
0012      C READ STATION IDENT, LAT DEGS, LAT MINS, LONG DEGS, LONG MINS
0013          READ (5,1) IDENT1,LATD,LATM,LONGD,LONGM
0014          1 FORMAT (10A1,4I10)
0015          L5=(LATD+LATM/60.)*R5
0016          L6=(LONGD+LONGM/60.)*R5
0017          10 CONTINUE
0018      C READ YEAR,MONTH,DAY,(START TIME GMT),(END TIME GMT),(TIME INCREMENT MINS),
0019      C (MAXIMUM ELEVATION DEGS )
0020          READ (5,2) Y,M,D,B,E1,I6
0021          2 FORMAT(7I10)
0022          IF(Y.EQ.U) STOP
0023          IF(I.EQ.U) I=10
0024          IF(I6.EQ.U) I6=100
0025          IF(E1.EQ.U) E1=2400
0026          I1=2
0027      C CALCULATE JULIAN DATE
0028          IF (M.GE.3) GO TO 16
0029          C1=-1
0030          IF ((Y-1853)/4).LT.11) C1=0
0031          J1=365*(Y-1853) + 30*(M+9) + ((M+10)/2) + D
0032          J2=((Y-1853)/4) + C1 + 1
0033          GO TO 27
0034      16 C1=-1
0035          IF ((Y-1852)/4).LT.11) C1=0
0036          IF (M.EQ.9.OR.M.EQ.11) GO TO 24
0037          C2=0
0038          GO TO 25
0039      24 C2=1
0040          GO TO 25
0041      25 J1=365*(Y-1852) + 30*(M-3) + ((M-2)/2) + D
0042          J2= ((Y-1852)/4) + C1 + C2
0043          J=J1+J2
0044      27 J=J1+J2

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0039      T1=FLOAT(J)-17472.5
0040      JD=FLOAT(J)+2397547.5
0041      WRITE (6,3) IDENT,LAT0,LATM,LANG0,LANGM,Y,M,O,JD
0042      3 FORMAT ('1 LUNAR COORDINATES FOR 1,10A1/1 STATION LAT: 1,214,1
+LONG: 1,214/1 OATE 1,14,1/1,12,1/1,12,1 JD=1,F12.1//')
0043      WRITE(6,5)
0044      5 FORMAT(' GMT AZ EL GHA DEC//')
0045      29 O9=B - (B/100)*100 + (B/100)*60
0046      D6= E1 - (E1/100)*100 + (E1/100)*60
0047      D7=D9-06
0048      D8=D7-I
0049      IF(D7.LE.0) GO TO 38
0050      IF(D8.GE.0) GO TO 10
0051      B=E1
C CALCULATE LUNAR LAT AND LONG
0052      38 T=FLOAT(B-(B/100)*100)/1440.+FLOAT(B/100)/24.
0053      T5=T1+T
0054      K1=FNB(0.751213+0.036601102*T5)
0055      K2=FNB(0.822513+0.0362916457*T5)
0056      K3=FNB(0.995766+0.00273777852*T5)
0057      K4=FNB(0.974271+0.0338631922*T5)
0058      K5=FNB(0.0312525+0.0367481957*T5)
0059      L8=K1+0.658*R5*SIN(2.*K4)+6.289*R5*SIN(K2)
0060      L8=L8-1.274*R5*SIN(K2-2.*K4)-0.186*R5*SIN(K3)
0061      L8=L8+0.214*R5*SIN(2.*K2)-0.114*R5*SIN(2.*K5)
0062      L8=L8-0.059*R5*SIN(2.*K2+2.*K4)-0.057*R5*SIN(K2+K3-2.*K4)
0063      K6=K5+0.6593*R5*SIN(2.*K4)+6.2303*R5*SIN(K2)-1.272*R5*SIN(K2-2.*K4)
0064      L7=5.144*R5*SIN(K6)-0.146*R5*SIN(K5-2.*K4)
C CALCULATION OF RA AND DEC
0065      D1=COS(L7)*SIN(L8)*0.397821+SIN(L7)*0.917463
0066      O1=ATAN2(O1,SQRT(1.-D1**2))
0067      A2=COS(L7)*COS(L8)/COS(D1)
0068      A1=(COS(L7)*SIN(L8)*0.917463-SIN(L7)*0.397821)/COS(O1)
0069      A=ATAN2(A1,A2)
0070      R1=A
0071      L1=0.065709822*T1
0072      L=T*24.*1.002738+6.646055+(L1-AINT(L1/24)*24.)
0073      L=(L-AINT(L/24)*24)
C CALCULATION OF GREENWICH HOUR ANGLE G FROM LOCAL SIDERIAL TIME
0074      G=(L/24)*P5-R1
0075      IF(G.LT.P5) GO TO 67
0076      G=G-P5
0077      GO TO 71
0078      67 IF(G.LT.0.) GO TO 69
0079      GO TO 71
0080      69 G=G+P5
C CALCULATION OF LOCAL HOUR ANGLE H FROM GHA
0081      71 H=L6-G
C CALCULATION OF ELEVATION E
0082      E3=COS(L5)*COS(H)*COS(O1)+SIN(D1)*SIN(L5)
0083      E2=SQRT(1-E3**2)
0084      E=ATAN2(E3,E2)
0085      IF(E.LT.0.) GO TO 117
0086      IF(E.GT.(16*R5)) GO TO 117
C CALCULATION OF AZIMUTH A
0087      A2=SIN(D1)/(COS(L5)*COS(E))
0088      A2=A2-(SIN(L5)/COS(L5))*(SIN(E)/COS(E))
0089      A1=SIN(L5)*SIN(D1)+COS(L5)*COS(O1)*COS(H)
0090      A1=(SIN(H)*COS(D1))/SQRT(1.-A1**2)
0091      A=ATAN2(A1,A2)
0092      AZ=FNA(A)
0093      EL=FNA(E)
0094      GHA=FNA(G)
0095      DEC=FNA(D1)
0096      GMT(1)=B/1000
0097      GMT(2)=B/100-(B/1000)*10
0098      GMT(3)=B/10-(B/100)*10
0099      GMT(4)=B-(B/10)*10
0100      IF((T-11).GT.(2.*I/1440.)) WRITE (6,7)
0101      7 FORMAT(1H )
0102      104 WRITE(6,6) GMT,AZ,EL,GHA,DEC
0103      6 FORMAT(3H ,4I1,4F12.1)
0104      I1=T
0105      117 B=B+I

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0106      Z=B-(B/100)*100 - 60
0107      IF(Z.LT.0) GO TO 29
0108      B=(B/100)*100 + 100 + Z
0109      GO TO 29
0110      END

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LUNAR COORDINATES FOR G3NAQ  
 STATION LAT: 51 34 LONG: 1 18  
 DATE 1978/ 5/20 JD# 2443648.0

| GMT  | AZ     | EL   | GHA   | DEC   |
|------|--------|------|-------|-------|
| 0000 | -143.7 | 24.3 | 34.2  | -7.7  |
| 0010 | -141.3 | 23.3 | 36.6  | -7.7  |
| 0020 | -138.9 | 22.4 | 39.0  | -7.7  |
| 0030 | -136.6 | 21.3 | 41.5  | -7.8  |
| 0040 | -134.4 | 20.3 | 43.8  | -7.8  |
| 0050 | -132.1 | 19.1 | 46.3  | -7.8  |
| 0100 | -129.9 | 18.0 | 48.7  | -7.8  |
| 0110 | -127.7 | 16.8 | 51.1  | -7.9  |
| 0120 | -125.6 | 15.6 | 53.4  | -7.9  |
| 0130 | -123.4 | 14.3 | 56.0  | -7.9  |
| 0140 | -121.4 | 13.0 | 58.4  | -7.9  |
| 0150 | -119.4 | 11.7 | 60.7  | -8.0  |
| 0200 | -117.4 | 10.4 | 63.1  | -8.0  |
| 0210 | -115.4 | 9.0  | 65.5  | -8.0  |
| 0220 | -113.3 | 7.6  | 68.0  | -8.0  |
| 0230 | -111.5 | 6.2  | 70.4  | -8.1  |
| 0240 | -109.6 | 4.8  | 72.8  | -8.1  |
| 0250 | -107.6 | 3.3  | 75.2  | -8.1  |
| 0300 | -105.8 | 1.9  | 77.6  | -8.2  |
| 0310 | -103.9 | 0.4  | 80.0  | -8.2  |
| 1720 | 107.2  | 0.1  | 285.0 | -10.5 |
| 1730 | 109.1  | 1.5  | 287.4 | -10.5 |
| 1740 | 111.0  | 2.8  | 289.7 | -10.5 |
| 1750 | 113.0  | 4.2  | 292.1 | -10.6 |
| 1800 | 114.9  | 5.5  | 294.6 | -10.6 |
| 1810 | 116.9  | 6.9  | 297.1 | -10.6 |
| 1820 | 118.9  | 8.1  | 299.4 | -10.6 |
| 1830 | 120.9  | 9.4  | 301.8 | -10.7 |
| 1840 | 122.9  | 10.7 | 304.2 | -10.7 |
| 1850 | 125.0  | 11.9 | 306.6 | -10.7 |
| 1900 | 127.1  | 13.1 | 309.0 | -10.7 |
| 1910 | 129.2  | 14.2 | 311.4 | -10.8 |
| 1920 | 131.4  | 15.4 | 313.9 | -10.8 |
| 1930 | 133.6  | 16.5 | 316.3 | -10.8 |
| 1940 | 135.8  | 17.5 | 318.7 | -10.8 |
| 1950 | 138.1  | 18.5 | 321.1 | -10.9 |
| 2000 | 140.4  | 19.5 | 323.5 | -10.9 |
| 2010 | 142.7  | 20.4 | 325.9 | -10.9 |
| 2020 | 145.0  | 21.2 | 328.3 | -10.9 |
| 2030 | 147.4  | 22.0 | 330.8 | -11.0 |
| 2040 | 149.9  | 22.8 | 333.2 | -11.0 |
| 2050 | 152.3  | 23.5 | 335.6 | -11.0 |
| 2100 | 154.7  | 24.1 | 337.9 | -11.1 |
| 2110 | 157.3  | 24.7 | 340.4 | -11.1 |
| 2120 | 159.9  | 25.2 | 342.8 | -11.1 |
| 2130 | 162.4  | 25.7 | 345.1 | -11.1 |
| 2140 | 165.0  | 26.1 | 347.5 | -11.1 |
| 2150 | 167.7  | 26.4 | 350.1 | -11.1 |
| 2200 | 170.3  | 26.7 | 352.5 | -11.2 |
| 2210 | 172.8  | 26.9 | 354.8 | -11.2 |
| 2220 | 175.5  | 27.0 | 357.2 | -11.2 |
| 2230 | 178.2  | 27.1 | 359.7 | -11.2 |
| 2240 | -179.1 | 27.0 | 2.0   | -11.3 |
| 2250 | -176.5 | 27.0 | 4.4   | -11.3 |
| 2300 | -173.8 | 26.8 | 6.8   | -11.3 |
| 2310 | -171.2 | 26.6 | 9.3   | -11.4 |
| 2320 | -168.6 | 26.3 | 11.7  | -11.4 |
| 2330 | -166.0 | 26.0 | 14.1  | -11.4 |
| 2340 | -163.4 | 25.5 | 16.5  | -11.4 |
| 2350 | -160.8 | 25.1 | 18.9  | -11.5 |
| 2400 | -158.3 | 24.5 | 21.3  | -11.5 |